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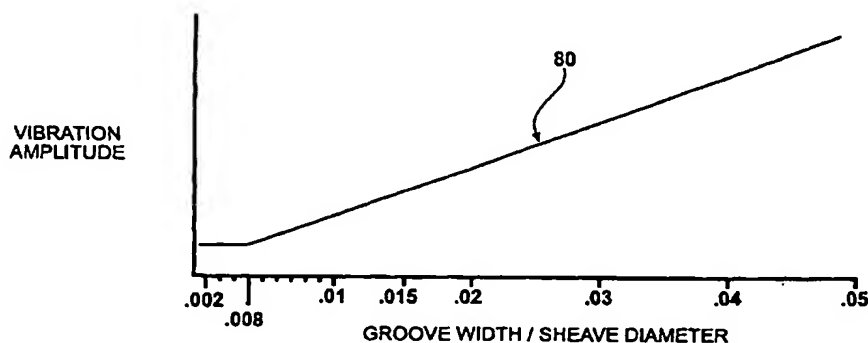
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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: ELEVATOR SYSTEM DESIGN INCLUDING A BELT ASSEMBLY WITH A VIBRATION AND NOISE REDUCING GROOVE CONFIGURATION



(57) Abstract: An elevator system design incorporates a belt having a jacket coating a plurality of elongate load bearing members such as steel cords. The jacket includes a plurality of spaced grooves on at least one side of the belt. The width of the grooves and the size of at least the drive sheave in the system are selected so that a ratio of the groove width to the sheave diameter is within a selected range. In one example, the ratio preferably is less than about .05. The grooves also preferably include a fillet at the edges of the grooves where the grooves meet with the sheave-engaging surface on the belt jacket.

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ELEVATOR SYSTEM DESIGN INCLUDING A BELT ASSEMBLY WITH A VIBRATION AND NOISE REDUCING GROOVE CONFIGURATION

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1. Field of the Invention.

This invention generally relates to elevator system design. More particularly,
this invention relates to an elevator system design strategy incorporating a belt
10 assembly having a specialized groove configuration.

2. Description of the Related Art.

Elevator systems typically include a cab and counterweight that move within a
hoistway to transport passengers or cargo to different landings within a building, for
example. A load bearing member, such as roping or a belt typically moves over a set
15 of sheaves and supports the load of the cab and counterweight. There are a variety of
types of load bearing members used in elevator systems.

One type of load bearing member is a coated steel belt. Typical arrangements
include a plurality of steel cords extending along the length of the belt assembly. A
jacket is applied over the cords and forms an exterior of the belt assembly. Some
20 jacket application processes result in grooves being formed in the jacket surface on at
least one side of the belt assembly. Some processes also tend to cause distortions or
irregularities in the position of the steel cords relative to the exterior of the jacket
along the length of the belt.

Figure 6, for example, illustrates both of these phenomena. As can be seen,
25 the spacing between the exterior of the jacket 200 and the cords 210 varies along the
length of the belt. As can be appreciated from the illustration, the cords 210 are set
within the jacket as if they comprise a series of cord segments of equal length

corresponding to the groove spacing. The illustration of Figure 6 includes an exaggeration of the typical physical cord layout for purposes of illustration. The actual distortions or changes in the position of the cords relative to the jacket outer surfaces may not be discernable by the human eye in some examples.

5 When conventional jacket application processes are used, the manner in which the cords are supported during the jacket application process tends to result in such distortion in the geometry or configuration of the cords relative to the jacket outer surfaces along the length of the belt.

While such arrangements have proven useful, there is need for improvement.

10 One particular difficulty associated with such belt assemblies is that as the belt moves in the elevator system, the grooves and the cord placement in the jacket interact with other system components such as the sheaves and generate undesirable noise, vibration or both. For example, as the belt assembly moves at a constant velocity, a steady state frequency of groove contact with the sheaves creates an annoying,
15 audible tone. The repeated pattern of changes in the cord spacing from the jacket outer surfaces is believed to contribute to such noise generation.

An alternative arrangement is required to minimize or eliminate the occurrence of vibrations or an annoying tone during elevator system operation. This invention addresses that need.

20

SUMMARY OF THE INVENTION

In general terms, this invention is an elevator system design including a belt having a plurality of grooves that have a configuration selected to minimize vibration and noise during elevator system operation.

An elevator system designed according to this invention includes a cab that carries passengers or cargo between landings within a building, for example. A belt supports the cab and facilitates movement of the cab. The belt has a plurality of spaced grooves on at least one side of the belt. At least one sheave over which the belt travels as the cab moves includes a diameter that is selected to have a relationship to the width of the grooves on the belt. The ratio of the groove width to the sheave diameter is chosen to be less than about .05.

In one example, the ratio between the groove width and the belt diameter is selected to be between about .001 and .015.

A method of designing an elevator system according to this invention includes selecting a diameter of at least the drive sheave that is responsible for moving the belt and cab within the hoistway. The width of the grooves is then selected such that a ratio of the groove width to the sheave diameter is less than about .05. The inventive belt assembly includes a plurality of cords extending generally parallel to a longitudinal axis of the belt. A jacket over the cords includes a plurality of grooves configured to minimize the occurrence of vibrations and noise during elevator operation.

In another example, the grooves have fillets near the sheave-engaging surface of the jacket. A radius of curvature of the fillets may be customized along with other system parameters to minimize vibrations and noise. In one example, the fillets have a radius of curvature between about .1 mm and about .5 mm.

The various features and advantages of this invention will become apparent to those skilled in the art from the following detailed description of the currently

preferred embodiments. The drawings that accompany the detailed description can be briefly described as follows.

BRIEF DESCRIPTION OF THE DRAWINGS

5 Figure 1 schematically illustrates a portion of an example belt assembly designed according to an embodiment of this invention.

Figure 2 is a cross-sectional illustration taken along the lines 2-2 in Figure 1.

Figure 3 is a schematic illustration of elevator system designed according to an embodiment of this invention.

10 Figure 4 graphically illustrates a feature of the inventive approach to elevator system design.

Figure 5 graphically illustrates the vibration causing effects of a relationship between the dimensions of a groove width and sheave diameter.

Figure 6 schematically shows a prior art belt.

15

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

20 Figures 1 and 2 schematically illustrate a belt assembly 20 that is designed for use in an elevator system. A plurality of cords 22 are aligned generally parallel to a longitudinal axis of the belt assembly 20. In one example, the cords 22 are made of strands of steel wire.

A jacket 24 covers over the cords 22. The jacket 24 preferably comprises a polyurethane-based material. A variety of such materials are commercially available and known in the art to be useful for elevator belt assemblies. Given this description,

those skilled in the art will be able to select a proper jacket material to suit the needs of their particular situation.

The jacket 24 establishes an exterior width and thickness of the belt assembly 20. In one example, the width of the belt assembly is 30 millimeters and the thickness is 3 millimeters. In the same example, the cords 22 have a diameter of 1.65 millimeters. The cords 22 preferably extend along the entire length of the assembly.

The jacket 24 includes a plurality of grooves 30 on at least one side 32 of the jacket 24. In the illustrated example, the grooves extend across the entire width of the belt assembly.

The grooves result from some manufacturing processes, many of which are well known in the art, that are suitable for formation of the belt assembly 20. In the example embodiment of Figures 1 and 2, the grooves have a configuration that is useful for reducing vibrations during elevator system operation.

In the illustrated example, the groove configuration includes a rounded edge or fillet 34 at each end of each groove where the groove joins the side 32 of the exterior of the jacket. The fillets 34 differ from conventional groove designs where a sharp edge typically existed where the groove met with the exterior surface 32 of the jacket 24. A rounded fillet reduces noise and vibration as each groove contacts a sheave about which the belt wraps during elevator system operation.

The radius of curvature for each rounded edge or fillet 34 in the inventive arrangement preferably is selected to minimize the amount of vibration occurring from the interaction between the belt assembly 20 and other elevator system components. Various factors affecting the radius of curvature selection include the distance or spacing between the grooves 30, the width W of each groove, the stiffness

characteristics of the jacket material and the thickness of the jacket material, which typically dictates the depth of each groove. In general, it is more preferable to have a larger radius of curvature, which tends to smooth out the transition between the side 32 of the jacket 24 and the grooves 30. A belt incorporating the inventive fillet design will include a fillet radius of curvature in the range from about 0.1 mm to about 0.5 mm. In one example, the radius of curvature for the fillets 34 is about 0.2 mm. In another example the radius is about 0.4 mm.

Another benefit of the fillet 34 is that it tends to reduce the sensitivity to shearing effects as the belt assembly 20 travels over the drive sheave 58. Because of the differing weights on the different sides of the drive sheave, a portion of the belt assembly 20 tends to be under greater load than the other portion on the opposite side of the drive sheave 58. This occurrence tends to introduce a shear effect on the jacket material 24. Incorporating fillets 34 on the groove 30 tends to reduce the sensitivity to this shearing effect and the contribution to vibration and noise generation during elevator system operation.

The width W of each groove 30 preferably is selected so that there is a relationship between the groove configuration and other components in the elevator system that provides optimal noise-reducing performance. Figure 3 schematically illustrates an example elevator system 50 including an inventive belt assembly 20. Of course, there are other types of elevator system arrangements that include sheaves about which ropes or belts travel and this invention is not limited to the example system arrangement, which is schematically shown for discussion purposes. The elevator system 50 includes a conventional counterweight 52 and cab 54 that move through a hoistway 56 in a conventional manner. The belt assembly 20 is operative to

support the loads of the counterweight 52 and cab 54 during system operation. The illustrated example includes a drive sheave 58 driven by a motor mechanism 60. Idle sheaves 62, 64 and 66 facilitate the desired movement of the cab 54 and counterweight 52 through the hoistway as needed to transport passengers or cargo
5 between landings within a building, for example.

The groove width W preferably is selected to have a dimensional relationship with at least the diameter of the drive sheave 58 of the system 50. In some situations, all sheaves within the system 50 will have the same diameter while in others there may be sheaves of varying sizes within the system. At least the relationship between
10 the groove width W and the size of the drive sheave (or sheaves, depending on the particular installation) is chosen to optimize the noise reducing properties of the belt assembly 20.

In general, a larger sheave diameter is preferred as the width W of the grooves 30 is increased. This invention includes the realization that relatively larger groove
15 widths W compared to smaller sheave diameters tend to produce more vibration and noise generation than arrangements having a desirable dimensional relationship.

Figure 4 graphically illustrates this phenomena in the graph 70. A first plot 72 shows the amount of vibration occurring in an example arrangement where the belt has dimensions consistent with the examples mentioned above. The amount of
20 vibration occurring when the sheave diameter is 75 millimeters is shown in the plot 72. The plot 74 represents the amount of vibration occurring when the sheave diameter is increased to 100 millimeters. The plot at 76 shows the amount of vibration occurring when the sheave diameter is further increased to 125 millimeters. Given the peak-to-peak amplitude of each of the plots 72, 74 and 76, it is apparent

that a larger sheave diameter for the given groove configuration and dimensions provides the least amount of vibration and, therefore, is the least likely to have noise generation during elevator system operation.

One factor that must be considered when selecting a sheave diameter and a groove width W is that a smaller sheave diameter may be preferred because it requires less torque and a less expensive machine including the motor mechanism 60. On the other hand, a larger sheave tends to increase the life of the belt assembly 20 and, according to this invention, tends to decrease the amount of vibration and noise generation during elevator system operation. Those skilled in the art who have the benefit of this description will be able to select appropriate dimensional relationships to meet the needs of their particular situation.

According to this invention, one preferred relationship between groove width W and sheave diameter preferably results in a ratio of the groove width W to the sheave diameter that is less than about .05. According to one example implementation of this invention, when the ratio exceeds .05, the amount of vibration is considered beyond an acceptable level. In another example, where the speed of elevator cab movement is lower, a higher ratio may be acceptable depending on the particular elevator system.

As can be appreciated from Figure 5, as the ratio of groove width to sheave diameter increases, the amount of vibration (and noise) increases. The plot 80 in Figure 5 shows an amplitude of vibrations on the Y axis with the ratio of groove width to sheave diameter on the X axis. When the ratio is below .008, the amount of vibration is effectively the same and is considered acceptable in many situations because that level of vibration does not tend to generate any audible noise within the

elevator system. As the ratio increases from .008 to .05, the amount of vibration increases in a generally linear fashion as can be appreciated from the plot.

One preferred range for the ratio of groove width to sheave diameter is below about .008. When the term “about” is used before a parameter in this description, it
5 should be interpreted to include amounts varying by almost a full unit more or less within a factor of ten. For example, “about .008” should be interpreted to at least include a range from .0071 to .0089 and “about .05” should be interpreted to at least include a range from .041 to .059.

A variety of ranges may be used depending on the particulars of a given
10 elevator system. Those skilled in the art who have the benefit of this description will be able to select the best ratio to meet the needs of their particular situation.

By combining the relationship between the groove width W and the size of the sheave (i.e., sheave diameter) and incorporating fillets 34 on the grooves 30, the inventive arrangement presents a substantial improvement in reducing vibration and
15 noise generation during elevator system operation.

In some examples it is preferred to minimize the width of the grooves 30. There is, however, a point where the width of the groove 30 cannot become any smaller because of manufacturing tolerances. This tolerance will vary depending on the particular material selected to form the jacket 24 and the tooling used in the
20 manufacturing process.

Additionally, it is believed that below a certain width, the noise reducing benefits of the inventive arrangement are not increased, as can be appreciated from Figure 5.

The particular width of each groove 30 that provides optimal noise reducing performance may also vary depending on other characteristics of a particular elevator system, including overall belt assembly size and sheave diameter, for example. The speed of movement of the belt assembly 20 within the elevator system is another
5 factor that affects the optimally selected groove width W. In general, according to this invention it is preferred to utilize ratios of groove width to sheave diameter in lower ranges for higher speed elevator systems compared to those of lower speeds. In other words, as elevator speed increases, the preferred ratio of groove width to sheave diameter decreases. Likewise, as elevator speed decreases, the acceptable range of
10 ratios of groove width to sheave diameter increases. Those skilled in the art who have the benefit of this description will be able to select appropriate groove width W and sheave diameter(s) to optimize the noise reducing characteristics within a particular installation.

The preceding description is exemplary rather than limiting in nature.
15 Variations and modifications to the disclosed examples may become apparent to those skilled in the art that do not necessarily depart from the essence of this invention. The scope of legal protection given to this invention can only be determined by studying the following claims.

CLAIMS

We claim:

1. A method of designing an elevator system having a belt with a plurality of grooves on one side of the belt that travels over at least a drive sheave, comprising the
5 steps of:
 - selecting a diameter of at least the drive sheave; and
 - selecting a width of the grooves on the belt such that a ratio of the groove width to the sheave diameter is less than about .05.
- 10 2. The method of claim 1, including selecting the sheave diameter and groove width such that the ratio is less than about .015.
3. The method of claim 1, including selecting the sheave diameter and groove width such that the ratio is less than about .008.
- 15 4. The method of claim 1, including selecting the sheave diameter and groove width such that the ratio is between .001 and .015.
5. The method of claim 1, including selecting the ratio of groove width to sheave
20 diameter based upon an expected speed of elevator cab travel.
6. The method of claim 5, including selecting the ratio to be in a first range when the expected speed is a first speed and selecting the ratio to be in a second higher range when the expected speed is a second, slower speed.

7. The method of claim 5, wherein the expected speed is approximately 1 m/s and including selecting the sheave diameter and the groove width such that the ratio is less than about .008.

5

8. The method of claim 1, including providing a fillet at the edges of each groove.

9. An elevator system, comprising:
a cab;
a belt that supports the cab and facilitates movement of the cab, the belt having a plurality of spaced grooves on at least one side of the belt; and
5 at least one sheave over which the belt travels as the cab moves, the sheave having a diameter that has a relationship to a width of the grooves on the belt so that a ratio of the groove width to the sheave diameter is less than about .05.
10. The system of claim 9, wherein the ratio is less than about .015.
- 10 11. The system of claim 9, wherein the ratio is less than about .008.
12. The system of claim 9, wherein the ratio is between .001 and .015.
- 15 13. The system of claim 9, including a fillet at the edges of each groove.
14. The system of claim 13, wherein the fillets each have a radius of curvature that is between about 0.1mm and about 0.5mm

15. An elevator belt assembly, comprising:

a plurality of cords aligned generally parallel to a longitudinal axis of the belt;

and

a jacket over the cords, the jacket including a plurality of grooves spaced
5 longitudinally on at least one side of the jacket, the grooves including a fillet near the
one side of the jacket.

16. The assembly of claim 15, wherein each fillet has a radius of curvature that is
the same.

10

17. The assembly of claim 15, wherein each fillet has a radius of curvature that is
between about 0.1mm and about 0.5mm.

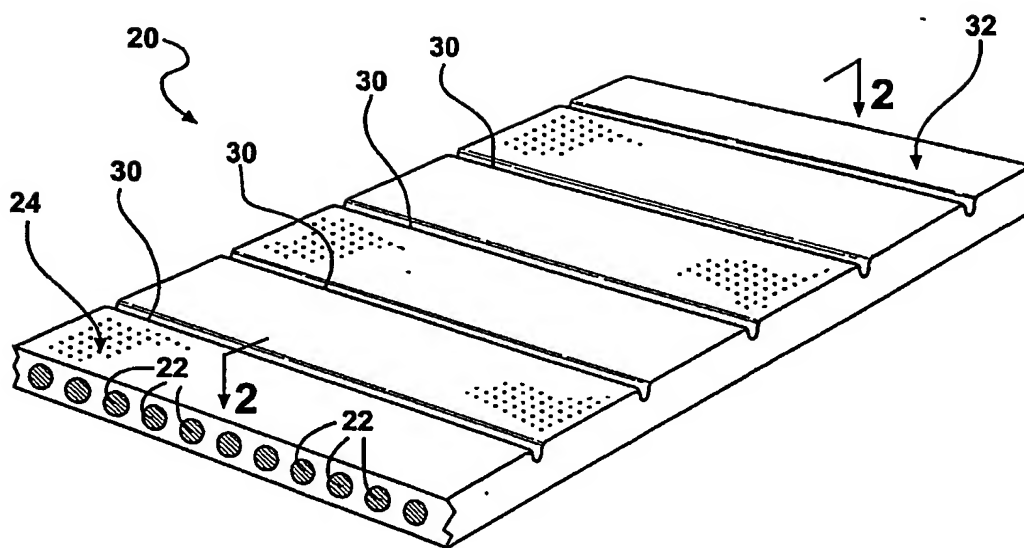
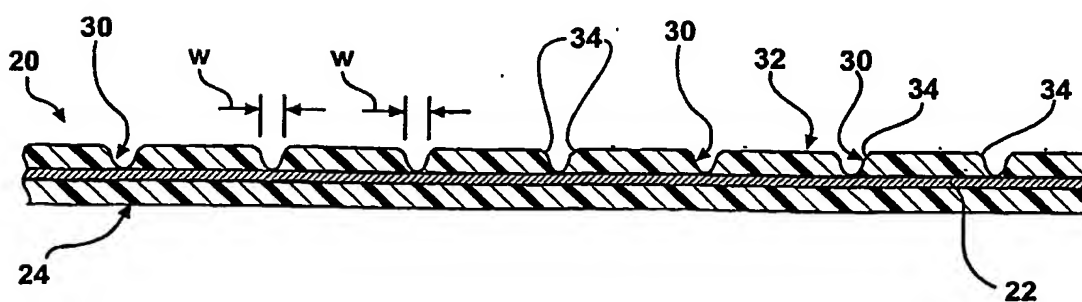
**FIG - 1****FIG - 2**

FIG - 3

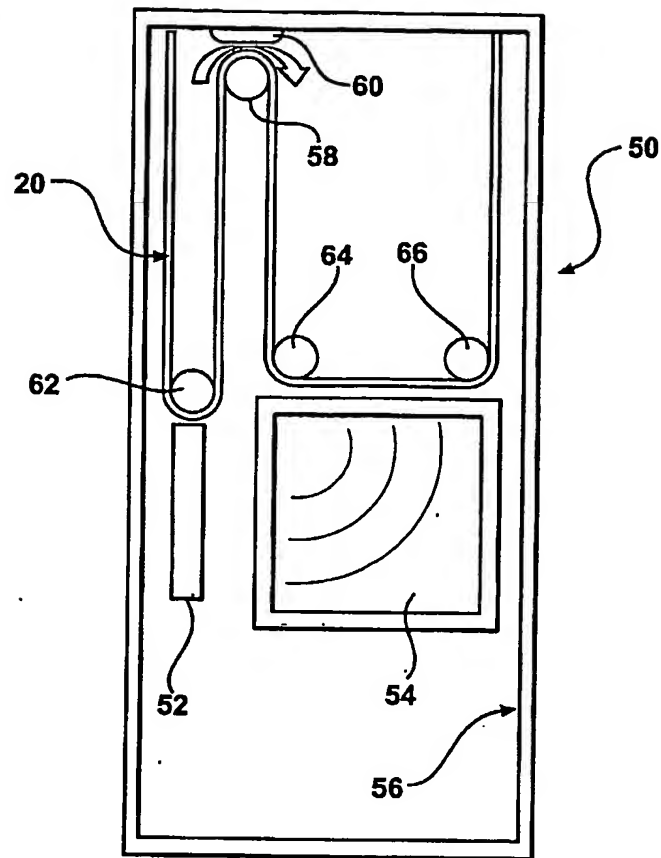
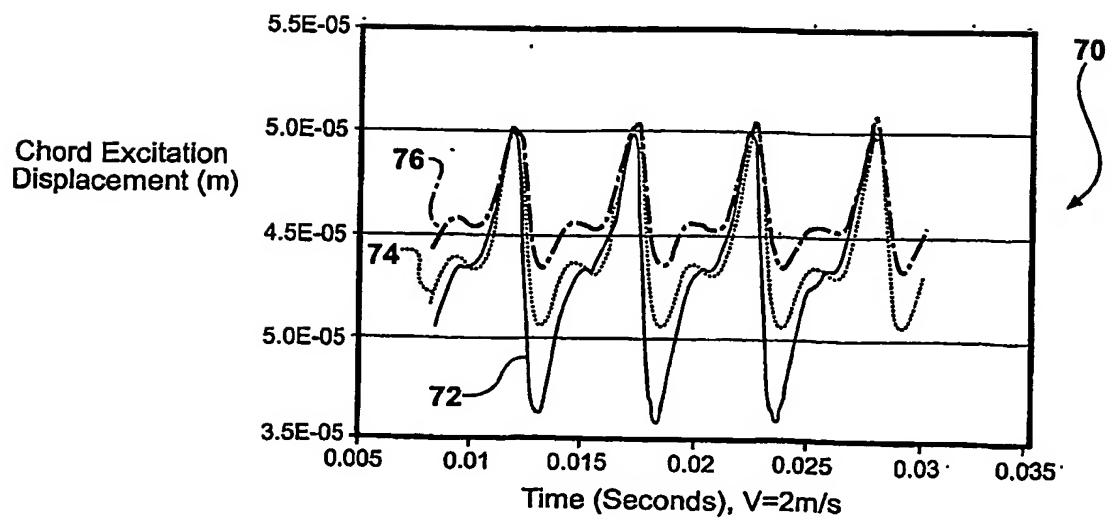
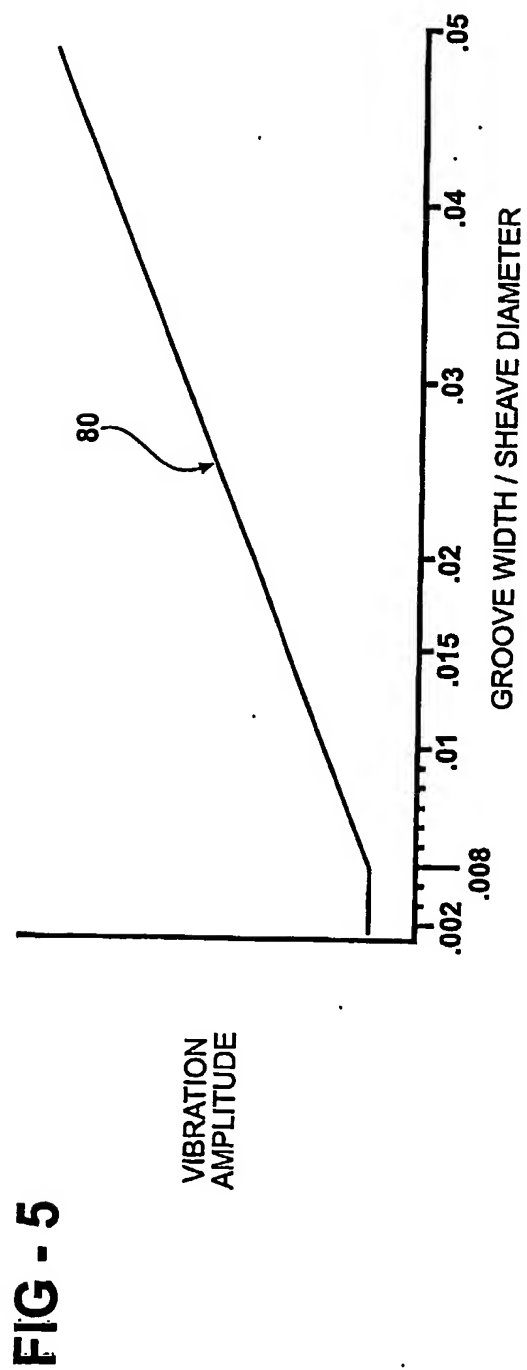


FIG - 4





INTERNATIONAL SEARCH REPORT

International application No.
PCT/US03/01148

A. CLASSIFICATION OF SUBJECT MATTER

IPC(7) :B66B 11/08, 7/06

US CL :187/251, 254

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 187/251, 254, 411, 414; 74/249, 250, 251

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	JP 4-345484 A (MITSUBISHI ELECTRIC CORP.) 01 December 1992 (01.12.1992), abstract and Figures 1-4.	1, 9
A	US 4,722,722 A (RAMPE) 02 February 1988 (02.02.1988), see whole document.	1
A	US 4,995,855 A (HASEBE et al.) 26 February 1991 (26.02.1991), see whole document.	1
A	US 5,308,291 A (ROBERTSON et al.) 03 May 1994 (03.05.1994), see whole document.	1

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	
"A" document defining the general state of the art which is not considered to be of particular relevance	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"E" earlier document published on or after the international filing date	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"O" document referring to an oral disclosure, use, exhibition or other means	"A" document member of the same patent family
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

19 MAY 2003

Date of mailing of the international search report

02 JUN 2003

Name and mailing address of the ISA/US
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INTERNATIONAL SEARCH REPORT

International application No.

PCT/US03/01148

Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This international report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☐ Claims Nos.:
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:
3. ☐ Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.
☐ No protest accompanied the payment of additional search fees.